

SYSTEM, METHOD AND APPARATUS FOR POLARIZATION MODE
DISPERSION COMPENSATION AND DEMULTIPLEXING POLARIZATION
MULTIPLEXED SIGNALS

The present invention relates to the field of demodulation techniques for optical communication systems and in particular although not exclusively to demodulation of polarization multiplexed signals.

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As is known polarization multiplexing (PolMUX) allows the transmission at the same carrier wavelength in the same optical fibre of two orthogonally polarized optical signals, thus doubling the spectral efficiency. In this manner it is possible to double the amount of data transmitted in a unit of time whilst occupying the same wavelength

10 band.

With reference to a Wavelength Division Multiplexing (WDM) system, the use of PolMUX can be viewed from two perspectives: the first being a 4-level transmission system allowing a doubling of the transmission rate per wavelength channel without changing the transmitted symbol speed (for example a 40Gbit/s channel can be

15 transmitted in the form of two 20Gbit/s orthogonally polarized optical signals), and the second a method of doubling the number of WDM channels without changing (reducing) the wavelength channel spacing.

20 Although promising, PolMUX presents considerable practical difficulties in implementing it in optical communications system. For example it is known that an optical signal which is transmitted over an optical fibres undergoes random time-

varying rotation to its state of polarization. As a result the state of polarization of the received optical signal is subject to random time-varying rotation. Although this phenomenon will not affect the orthogonality of the two polarization multiplexed signals it will affect the orientation with the orthogonal states of polarization are
5 presented to the receiver thus making their separation impossible without an appropriate dynamic polarization tracking technique.

Moreover, in the case of high-speed symbol transmission systems, Polarization Mode Dispersion (PMD) will widen, distort and depolarize the transmitted pulses and cause
10 considerable deterioration in the quality of the received signal. PMD can also give rise to mutual interference and mixing of the two orthogonal polarization signals.

The present invention arose in an endeavour to at least in part remedy the above mentioned shortcomings and provides a system that allows simultaneous PMD
15 compensation and demultiplexing of polarization multiplexed signals.

In accordance with a first aspect of the invention there is provided a transmission system comprising two optical signals transmitted over the same fibre at the same wavelength but with orthogonal polarization and characterised by receiving apparatus
20 capable of filtering the two components with orthogonal polarization of the signal received in accordance with a transfer matrix which is controlled dynamically on the basis of the output signals in such a manner as to approximate the reverse transfer matrix of the fibre in the region of the spectrum occupied by the signal so as to compensate for the PMD and the polarization rotation introduced by the fibre and

eliminating distortion and mutual interference effects for both the signals and obtaining at output an approximate repetition of the two signals transmitted.

In accordance with a second aspect of the invention there is provided a transmission
5 method comprising two optical signals transmitted over the same fibre at the same wavelength but with orthogonal polarization and characterised by at the receiving side filtering the two components with orthogonal polarization of the signal received according to a transfer matrix and dynamically controlling the transfer matrix on the basis of the signals output in such a manner as to approximate the reverse transfer
10 matrix of the fibre in the region of the spectrum occupied by the signal so as to compensate for the PMD and the polarization rotation introduced by the fibre while eliminating distortion and mutual interference effects for both the signals and obtaining at output an approximate repetition of the two signals transmitted.

15 In accordance with a further aspect of the invention there is provided an apparatus for receiving an polarization multiplexed optical signal transmitted over a fibre and made up of two polarization multiplexed signals and to perform simultaneous compensation of the polarization mode dispersion (PMD) and demultiplexing of the two signals and characterised by means which filter the two orthogonal polarization components of the
20 signal received according to a transfer matrix which is controlled dynamically on the basis of the signals output in such a manner as to approximate the reverse transfer matrix of the fibre in the region of the spectrum occupied by the signal so as to compensate for the PMD and the polarization rotation introduced by the fibre while

eliminating distortion and mutual interference effects for both the signals and obtaining at output an approximate repetition of the two signals transmitted.

In order that the invention can be better understood embodiments in accordance with the invention will now be described by way of example only with reference to the accompanying drawings in which:

Figure 1 is a block diagram of a polarization multiplexing transmission system in accordance with the invention;

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Figure 2 is a functional block diagram of the demultiplexing DMUX apparatus of Figure 1 as a combination of transversal filters with complex coefficients;

Figure 3 is a practical implementation of the DMUX apparatus of Figure 2 implemented in the form of a Planar Lightguide Circuit (PLC);

Figure 4 shows another possible implementation of the DMUX of Figure 2 using Polarization Controllers (PC) and Polarization Maintaining Fibres (PMF);

Figure 5 is a block diagram of the transfer functions to which the signals are subjected in the system of Figure 1;

Figure 6 are two channel eye diagrams before (left hand side) and after (right hand side) filtering by the planar lightguide circuit (PLC); and

Figure 7 plots of outage probability versus normalised mean differential group delay (DGD) for the polarisation multiplexing system of the invention compared to an uncompensated on off keying (OOK) and first order compensated OOK systems.

5 Referring to Figure 1 there is shown a Polarization multiplexing transmission system (designated as a whole by reference number 10) in accordance with the invention. In particular, the dashed-line rectangle 11 shows the receiver stage in accordance with the invention for simultaneously compensating for polarization mode dispersion and demultiplexing the received polarization multiplexed optical signal.

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At the transmitter end 12, two independent bit streams a_1 and a_2 are applied to two respective transmitters TX 13 which produce corresponding intensity modulated optical signals z_1 and z_2 with the same carrier wavelength λ . The transmitter 13 conveniently comprises a single laser for generating the optical carrier, an optical splitter for splitting
15 the laser light and a respective optical modulator for modulating light from the laser with the bit streams a_1 and a_2 . The two modulated optical signals z_1 and z_2 of carrier wavelength λ are combined such that their respective states of polarization are orthogonal to one another by a Polarization Beam Combiner (PBC) 14 and the polarization multiplexed signal transmitted through an optical fibre 15 to the receiving
20 stage 11.

In the receiver 11 the received polarization multiplexed signal is separated into two orthogonal components by a Polarization Beam Splitter (PBS) 16 whose axes are arbitrarily oriented. The two separated components x_1 and x_2 are applied to a respective

input port of a demultiplexing (DMUX) device 17 to produce components y_1 and y_2 at respective output ports of the device. The DEMUX device 17 will be described in detail below and can be fabricated in the form of a Planar Lightguide Circuit (PLC) or as a cascade of discrete components such as Polarization Controllers and Polarization
5 Maintaining Fibres.

As will be shown, by appropriate configuring and control of the filtering function of the DEMUX device 17 the two output components y_1 and y_2 correspond to the two transmitted signals z_1 and z_2 appropriately equalized and demultiplexed to compensate
10 for the effects of the propagation through the fibre 15.

The components y_1 and y_2 are detected by a respective photodetector 18 to produce corresponding electrical signals s_1 and s_2 which are input to known receiver (RX) 19. The receivers 19 produce respective output signals \hat{a}_1 and \hat{a}_2 which by appropriate
15 configuration and control of the DMUX will correspond to the original bit stream signals a_1 and a_2 . The receivers 19 for the two channels can be completely separate or share some elements such as the clock recovery circuit.

As will be clarified below, the DMUX device 17 is advantageously adaptively
20 controlled by continually updating the value of its control parameters on the basis of a feedback signal derived from the signals s_1 , s_2 , \hat{a}_1 and \hat{a}_2 . A control circuit 20 controls the DMUX device control parameters on the basis of a feedback signal which is generated by a block 21 which calculates said signal on the basis of the characteristics

of the signals s_1 , s_2 , \hat{a}_1 and \hat{a}_2 . An advantageous realization of the feedback control arrangement is explained below.

Figure 2 shows a functional diagram of the demultiplexing DMUX device 17 by means
 5 of a combination of a plurality N of transverse filters with complex coefficients that are indicated below as two-dimensional filters. The DMUX device has transfer function $H(\omega)$ given by:

$$H(\omega) = e^{-j\frac{N}{2}\omega\tau} \begin{pmatrix} C(\omega) & D(\omega) \\ -D^*(\omega) & C^*(\omega) \end{pmatrix} \quad (1)$$

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The two functions $C(\omega)$ and $D(\omega)$ can be represented by means of their Fourier series expansion ($N+1$ terms):

$$15 \quad C(\omega) = \sum_{k=0}^N c_k e^{-j(k-N/2)\omega\tau} \quad (2)$$

$$D(\omega) = \sum_{k=0}^N d_k e^{-j(k-N/2)\omega\tau} \quad (3)$$

where c_k and d_k are complex coefficients. It is known that such filters have periodic
 20 transfer functions, with a period $1/\tau$, whose course can be controlled by appropriately changing the coefficients. The only limits are set by the periodicity of the transfer

functions and the finite number, $N+1$, of harmonics representing them. In addition, to have a unitary transfer matrix there is the additional constraint that:

$$|C(\omega)|^2 + |D(\omega)|^2 = 1 \quad (4)$$

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Figure 3 shows a schematic representation of a possible implementation of the DMUX device 17 that is implemented as a Planar Lightguide Circuit (PLC). The device 17 is a 4-port device, two input and two output ports, and comprises a cascade of N identical filtering elements. Each element comprises an interferometric structure which includes within the first optical path: a delay line 21 which introduces a delay τ to optical signals passing along the first path relative to the second path and a phase modulator 22 controlled by a parameter ϕ_n (where $n= 1$ to N). Each filtering element further comprises a variable coupler 23 controlled by a parameter θ_n for coupling optical signals from the first and second paths. At the input of the device 17 there a further variable coupler θ_0 is provided. Implementation of each of the components within the DMUX device will be readily imaginable to one skilled in the art, and can comprise for example a Mach-Zehnder interferometer type structure. The total number of controllable parameters is $Q=2N+1$ which is the number of degrees of freedom of the device 17. To enhance the dynamic functioning of the device it is also possible that some, or all, of the N elements of the device include a larger number of phase modulators 22 and variable couplers 23 to increase the number of degrees of freedom of the device. The overall transfer matrix of the device can be calculated by multiplying the transfer matrices of the individual elements. In particular, by omitting an unessential

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delay phase term, the transfer matrix of the variable coupler H_{θ_n} , phase modulator H_{ϕ_n} and delay line $H_{\tau}(\omega)$ are respectively:

$$H_{\theta_n} = \begin{pmatrix} \cos \theta_n & -j \sin \theta_n \\ -j \sin \theta_n & \cos \theta_n \end{pmatrix}$$

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$$H_{\phi_n} = \begin{pmatrix} e^{j\phi_n/2} & 0 \\ 0 & e^{-j\phi_n/2} \end{pmatrix}$$

$$H_{\tau}(\omega) = \begin{pmatrix} e^{-j\omega\tau/2} & 0 \\ 0 & e^{j\omega\tau/2} \end{pmatrix} \quad (5)$$

10 Accordingly, the overall transfer matrix $H(\omega)$ for the DEMUX device 17 is given by:

$$H(\omega) = \left[\prod_{n=N}^1 (H_{\theta_n} H_{\phi_n} H_{\tau}(\omega)) \right] H_{\theta_0} \quad (6)$$

It can be shown that the transfer matrix (6) is a frequency-dependent unitary transfer
 15 matrix that can be written in the same form indicated by equations (1) to (4).
 Accordingly, the PLC (Planar Lightguide Circuit of Figure 3) device realizes the
 functionality requested of the DMUX 17 device. In practice, it is necessary to allow for
 the fact that the control parameters will not be directly the complex coefficients of the
 transverse filter but the Q parameters of the PLC linked thereto non-linearly. This does
 20 not present a problem for realization of the present invention.

Figure 4 illustrates an alternative implementation of the DMUX 17 using cascaded polarization controllers (PC) and polarization maintaining fibres (PMF).

From a systems theory viewpoint the description of this device is identical to that of the PLC device of Figure 3. The above equations (5) and (6) and the deriving consequences are thus equally valid considering that to spatial separation of the input and output signals of the PLC correspond in this case a polarization separation and that the PBS at the input of the DMUX device in Figure 1 must be shifted to the output of the apparatus.

The operating principle of the DMUX 17 apparatus is based on the controllability of its transfer matrix. In the event of choosing a value of τ sufficiently small (for example half of the bit period of the input signal) and having a sufficiently large number N of stages (4 stages, for example) the device is capable of approximating the reverse transfer matrix of the fibre in the region of the spectrum occupied by the signal.

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In this manner the two output signals are essentially an (approximate) reproduction of the signals transmitted.

With reference to the block diagram of Figure 5 the vectors:

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$$\begin{pmatrix} Z_1(\omega) \\ Z_2(\omega) \end{pmatrix}, \begin{pmatrix} X_1(\omega) \\ X_2(\omega) \end{pmatrix}, \begin{pmatrix} Y_1(\omega) \\ Y_2(\omega) \end{pmatrix} \quad (7)$$

respectively represent in the frequency domain the pair of signals z_1 and z_2 at the input of the fibre, x_1 and x_2 at the output of the fibre and y_1 and y_2 at the output of the DMUX.

Thus the following relationships can be written:

$$\begin{pmatrix} Y_1(\omega) \\ Y_2(\omega) \end{pmatrix} = H(\omega) \begin{pmatrix} X_1(\omega) \\ X_2(\omega) \end{pmatrix} \quad (8)$$

5 and

$$\begin{pmatrix} X_1(\omega) \\ X_2(\omega) \end{pmatrix} = U(\omega) \begin{pmatrix} Z_1(\omega) \\ Z_2(\omega) \end{pmatrix} \quad (9)$$

In equation (9), $U(\omega)$ represents the Jones matrix of the optical fibre 15 and allows for the rotation effects and Polarization Mode Dispersion (PMD) with a reference system which at input is aligned with the axes of the Polarization Beam Combiner (PBC) and at the output to those of the Polarization Beam Splitter (PBS).

In the above event in which the device approximates the reverse transfer matrix we can write:

$$15 \quad H(\omega) \cong U^{-1}(\omega) \quad (10)$$

and the following relationship then applies

$$\begin{pmatrix} Y_1(\omega) \\ Y_2(\omega) \end{pmatrix} = H(\omega) U(\omega) \begin{pmatrix} Z_1(\omega) \\ Z_2(\omega) \end{pmatrix} \cong \begin{pmatrix} Z_1(\omega) \\ Z_2(\omega) \end{pmatrix} \quad (11)$$

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From equation (11) the result is that the two signals y_1 and y_2 at the output of the device 17 are approximately a reproduction of the two transmitted signals z_1 and z_2 . It follows

that, photodetecting and sending said signals to the respective receiver 19, the two sequences of received symbols \hat{a}_1 and \hat{a}_2 are the same as the sequences of transmitted symbols a_1 and a_2 .

5 An example of operation of the DMUX device 17 is shown in Figure 6, which shows two channel eye diagrams before (left hand side) and after (right hand side) filtering by the DMUX device 17. In Figure 6 the DMUX device is fabricated in form of a planar lightwave circuit (PLC) and the eye diagrams are for PolMUX transmission over a fibre affected by Polarization Mode Dispersion (PMD). The eye diagrams for both channels
10 are shown at for the input and output of the DMUX. From a comparison of the eye diagrams it is evident that the distortion and mutual interference caused by the PMD are virtually totally eliminated by the DMUX device.

The performance obtainable by means of the transmission system in accordance with
15 the present invention can be given in terms of penalization of the optical-signal to noise ratio (OSNR) and outage probability (OP). A standard On Off Keying OOK system is considered for comparison purposes. OSNR penalization refers to an OOK system in a back-to-back configuration for a 10^{-12} Bit Error Rate (BER). OP is the probability that the OSNR penalization will become greater than 3 dB.

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A quantitative estimate of the performance of the system is shown in Figure 7 showing the outage probability as a function of the mean Differential Group Delay (DGD) of the connection that is a characterizing parameter of the statistical behaviour of a fibre in PMD terms.

In Figure 7, one of the two channels (they have the same outage probability) of a PolMUX system with 4-stage ($N=4$) DMUX is compared both with an uncompensated OOK system and with the same OOK system with exact compensation of the PMD of the first order.

As may be seen, the PolMUX channel obtained in accordance with the present invention has decidedly better performance and shows that the device of the present invention is actually capable of demultiplexing the two channels and performing a compensation of the PMD even for orders higher than the first. In particular, the proposed system can operate with mean DGD up to $0.42T_b$, keeping the OP below 10^{-6} . As mentioned above, it is advantageous and preferable in accordance with the present invention that during normal functioning of the system the DMUX device parameters are updated dynamically in such a manner as to follow the temporal variations of the transmission channel which are translated into changes in the fibre transfer matrix.

For this purpose, a feedback signal which is a good indicator of the quality of the signals received, i.e. the corresponding error rate, is used to control the parameters. In the present invention, the feedback signal is advantageously an estimate of the overall Mean Square Error (MSE) on the two signals received s_1, s_2 (the sum or, equivalently, the mean square value of the MSE of each of the two signals). This is determined by the processing block 21.

Alternatively the DMUX device can advantageously be controlled in response to other feedback signals, such as for example the sum (or mean value) of the openings of the eye diagrams (eye opening).

- 5 For the first of the two channels, the Mean Square Error MSE_1 is the expected value of the square of the difference between the value of the received signal $s_1(t_i)$, at the generic instant of sampling t_i , and the corresponding transmitted symbol a_{1i} :

$$MSE_1 = E \left\{ (s_1(t_i) - a_{1i})^2 \right\} \quad (12)$$

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Similarly, for the second channel:

$$MSE_2 = E \left\{ (s_2(t_i) - a_{2i})^2 \right\} \quad (13)$$

- 15 A good estimate of the two magnitudes can be obtained by substituting in equations (12) and (13) the transmitted symbols a_{1i} and a_{2i} with the corresponding symbols in reception \hat{a}_{1i} and \hat{a}_{2i} and the expected value with an average of a finite number M of samples. In this manner, considering taking the mean value of the MSEs for the two channels, the feedback signal is

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$$U(t_i) = \frac{1}{2M} \sum_{k=0}^{M-1} \left[(s_1(t_i - kT_b) - \hat{a}_{1(i-k)})^2 + (s_2(t_i - kT_b) - \hat{a}_{2(i-k)})^2 \right] \quad (14)$$

Considering a value of M sufficiently large, in the case in which the system is functioning correctly and the error rate is consequently very low, U is an excellent

approximation of the MSE. In practice, the operations indicated in equation (14) are performed inside the block 21 indicated MSE in Figure 1 which can be integrated or not in the receiver as will be readily imaginable to those skilled in the art.

5 Lastly, in control block 20 a minimization algorithm based on the gradient method is advantageously implemented. The Q parameters of the DMUX 17 are continually updated on the basis of this algorithm such as to minimize the feedback signal. To achieve the purpose, various algorithms can be used as will be readily imaginable to those skilled in the art, such as the algorithm of Newton and its derivatives, the
10 algorithm of Levenberg-Marquardt or the random algorithms like 'simulated annealing'.

The details of an advantageous usable algorithm, the manner in which the gradient is estimated and the law with which the parameters are updated are disclosed in our co-pending European patent application EP1456980 (Application No. 02788441.0) the
15 content of which is hereby incorporated by way of reference thereto.

It is now clear that the objectives of the invention have been achieved. The above description of an embodiment applying the innovative principles of the present invention is given by way of non-limiting example of said principles and variations can
20 be made that are within the scope of the invention.

Although in the foregoing description the two signals a_1 and a_2 are described as being mutually independent, that is they correspond to two distinct communications data streams, they can also be taken as decoding signals (for example multilevel) of a signal

to be transmitted. It will be clear to those skilled in the art that in this case the two received signals \hat{a}_1 and \hat{a}_2 can be used to obtain reverse decoding and recover the transmitted signal.

- 5 Equations (10) and (11) are indicative of the fact that the present invention can be used for various alternative modulation formats. Notwithstanding the modulation format used, the vectors defined in (7) can be respectively considered as the Jones representation of the field at the fibre input, the Jones representation of the corresponding field at the fibre output, and the Jones representation of the field at the
10 output of the DMUX assuming that the signals on the two outputs of the DMUX are the two orthogonal polarizations of the same field.

In the case explained above in which the DMUX 17 device is implemented a sequence of Polarization Controllers (PCs) and Polarization Maintaining Fibres (PMFs), this
15 formal artifice is not necessary, since the two outputs of the device being actually made up of the two signal polarizations.

Because of the phenomena described above, distortions present on the field at the fibre output can be such as to not allow correct decoding of the modulation format used. Use
20 of the present invention, allowing reversal of the fibre transfer matrix essentially allows eliminating the harmful effects of the channel by giving back at output a signal approximately identical to the one transmitted even from the viewpoint of the polarization state. In this manner the signal can be correctly decoded.

A practical example of the foregoing is made up for example of the modulation of the polarization state of the signal (known as multilevel PolSK modulation). With this type of modulation the PMD or even a simple polarization rotation are very detrimental. By using the present invention it is possible to compensate for both the polarization rotation
5 effects and the PMD effects by filtering the signal at the fibre output in accordance with the same diagram indicated for the PolMUX and sending the two DMUX outputs to a receiver for the PolSK format such as for example a known Stokes parameter receiver.

In this case the feedback signal is an estimate of the MSE mediated on all the channels
10 associated with the modulation. For example, considering a PolSK eight-level modulation, three different channels are associated with the three Stokes parameters of the optical signal. The MSE is then estimated for each of the three channels received and mediated on them.

Moreover although it is found advantageous to fabricate the DMUX device as a planar
15 lightwave circuit, other devices or series of devices providing an equivalent transfer matrix can be used. For example, it can comprise polarization controllers and polarization maintaining fibres such as described in the above-mentioned European Patent Application number EP1456980 followed by another polarization controller and
20 polarization divider as will readily be imaginable to those skilled in the art in the light of the explanations given herein.

As mentioned above, for dynamic control of the device, in the present invention reference is advantageously made to a particular feedback signal, the mean square error

MSE, and a particular minimization algorithm, the gradient algorithm. Other feedback signal capable of monitoring the quality of the two channels received as well as another minimization or maximization algorithm can be used.